

**APPLICATION FOR A CERTIFICATE OF APPROPRIATENESS FOR
A SIGN IN A SPECIAL PROVISION SIGN DISTRICT (SPSD)**

JEFFERSON AREA SPECIAL PURPOSE DISTRICT

CASE NUMBER: SIGN-26-000612

DATE FILED: Mar. 26th, 2026

LOCATION: 200 W JEFFERSON BLVD, STE A
(EAST ELEVATION)

SIZE OF REQUEST: 180 sq. ft.

COUNCIL DISTRICT: 1

ZONING: PD-316, Subarea 1

APPLICANT: Solon Carver of M3 GRAPHICS INC.

OWNER: 200 Jeff, LLC.

TENANT: Growth Wireless, LLC

REQUEST: An application for a Certificate of Appropriateness by Solon Carver of M3 GRAPHICS INC., for a 180-square-foot LED illuminated channel letter sign at 200 W JEFFERSON BLVD, STE A (EAST ELEVATION).

SUMMARY: The applicant proposes to install a 180-square-foot LED illuminated sign, composed of back lit aluminum channel letters on an aluminum backer panel that also incorporate a halo glow. Faces will be white acrylic with painted aluminum returns. Sign will read 'TOTAL WIRELESS'

STAFF RECOMMENDATION: Approval.

SSDAC RECOMMENDATION: Approval, subject to conditions.

BACKGROUND:

- The subject site is located in Jefferson Area Special Purpose District and is zoned Mixed Use Projects (MUP), a business zoning sign district.
These regulations are established in: [Sec. 51P-316.113](#) (Specific details included below).
- The applicant proposes to install a 180-square-foot LED illuminated sign, composed of back lit aluminum channel letters on an aluminum backer panel that also incorporate a halo glow. Faces will be white acrylic with painted aluminum returns. Sign will read 'TOTAL WIRELESS'.
 - The sign is composed of 3" aluminum channel letters, painted red with white acrylic faces, back-lit by LED, mounted to a 1.5" inches off of a flat aluminum backer panel. Sign elements are constructed entirely of metal, acrylic, and LED.
- This is the second sign location submitted for this site. The first location, (FRONT SIGN) was previously approved with conditions by SSDAC/CPC (Case# SIGN-25-002198) .
- This sign is to be mounted on the façade facing S Zang Blvd.
- Construction of the proposed sign is in accordance with SPSD regulations and meets the requirements of the Dallas City Code per Sec. 51P-316.113.

51P-316.113(a) PURPOSE.

The purpose of this article is to regulate both the construction of new signs and the alterations of existing signs with a view towards enhancing, preserving, and developing the unique character of this district. These sign regulations have been developed with the following objectives in mind:

- (1) To protect the historical and architectural character of this district from inappropriate signs in terms of number (clutter), style, color and materials.
- (2) To ensure that significant architectural features in this district or of a building within this district are not obscured.
- (3) To promote the economic success of each business within this district and, in turn, the collective success of this district.
- (4) To ensure that the size and orientation of signs are geared toward the high number of pedestrians in this district.
- (5) To enhance the aesthetics of this district.

51P-316.113(e) ATTACHED SIGNS.

(1) Attached signs in general.

(A) Except as provided in this paragraph and except for marquee signs, awning signs, and blade signs all attached signs must be mounted parallel to the building surface to which they are attached and may not project more than 18 inches from that building.

This sign meets all requirements of PD-316 and Article VII.

51A-7.505 PERMIT PROCEDURES FOR SPECIAL PROVISION SIGN DISTRICTS.

(B) **Factors the committee shall consider.** In reviewing an application, the committee shall first consider whether the applicant has submitted sufficient information for the committee to make an informed decision. If the committee finds the proposed sign to be consistent with the special character of the special provision sign district, the committee shall make a recommendation of approval to the city plan commission. **The committee shall consider the proposed sign in terms of its appropriateness to the special provision sign district with particular attention to the effect of the proposed sign upon the economic structure of the special provision sign district and the effect of the sign upon adjacent and surrounding premises without regard to any consideration of the message conveyed by the sign.** After consideration of these factors, the committee shall recommend approval or denial of the application and forward that recommendation to the city plan commission.

(6) Decision by the commission. Upon receipt of a recommendation by the committee, the commission shall hold a public hearing to consider the application. At least 10 days before the hearing, notice of the date, time, and place of the hearing, the name of the applicant, and the location of the proposed sign must be published in the official newspaper of the city and the building official shall serve, by hand-delivery or mail, a written notice to the applicant that contains a reference to this section, and the date, time, and location of this hearing. A notice sent by mail is served by depositing it properly addressed and postage paid in the United States mail. In addition, if the application is for a detached sign or for an attached sign that has more than 100 square feet of effective area, the applicant must post the required number of notification signs in accordance with Section 51A-1.106. **In making its decision, the commission shall consider the same factors that were required to be considered by the committee in making its recommendation.** If the commission approves the application, it shall forward a certificate of appropriateness to the building official within 15 days after its approval. If the commission denies the application, it shall so inform the building official in writing. Upon receipt of the written denial, the building official shall so advise the applicant within five working days of the date of receipt of the written notice.

Property Ownership

200 Jeff, LLC.
45 Main Street, Suite 506
Brooklyn, NY 11120

Officer names: Benjamin Atkins, Manager

Tenant Ownership

Growth Wireless, LLC
9404 W Sam Houston PKWY, Suite D
Houston, TX 77099

Officer names: Hakeem El-Ali, District Manager
Syed Abidi, Operations Manager

SSDAC Action:

April 14, 2026

MOTION: It was moved to **approve subject to conditions:**

An application for a Certificate of Appropriateness by Solon Carver of M3 GRAPHICS INC., for a 180-square-foot LED illuminated channel letter sign at 200 W JEFFERSON BLVD, STE A (EAST ELEVATION).

Maker: Hardin
Second: Webster
Result: Carried: 3 to 0

For: 3 - Peardon, Hardin and Webster
Against: 0 - none
Absent: 2 - Dumas and Coffman
Conflict: 0 - none

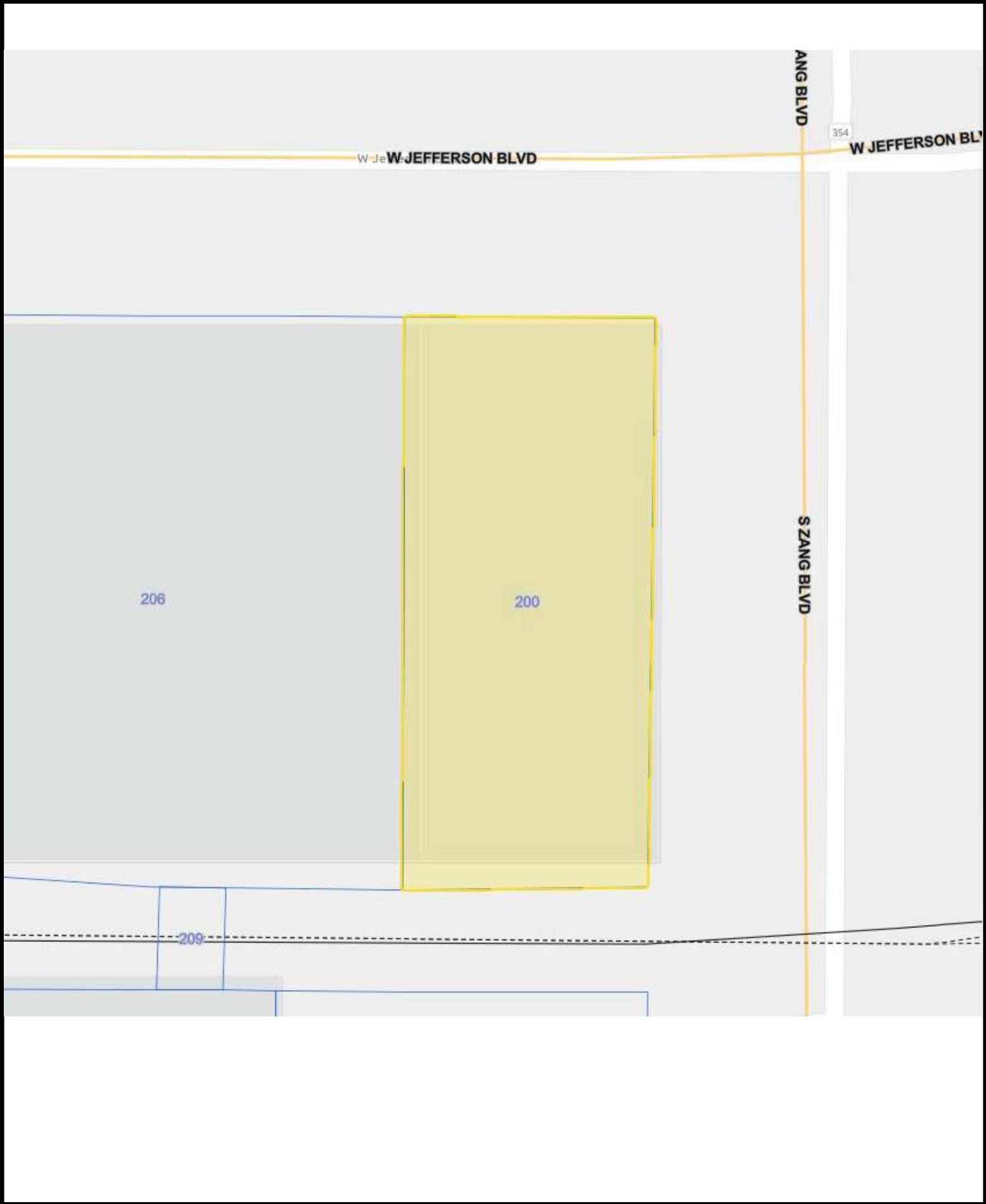
Speakers: none



Printed Date: 4/13/2026



Aerial Map - 200 W Jefferson Blvd



Printed Date: 4/13/2026



Zoning Map - 200 W Jefferson Blvd

SITE MAP



**COMPANY NAME /
PROJECT NAME**

Total Wireless

ADDRESS

**200 W Jefferson Blvd
Dallas, TX 75208**

**PROJECT MANAGER:
AARON VALVERDE**

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SIGN SPECIFICATIONS

Dual Lit channel letters mounted on an aluminum panel with separators

180 sq.ft.



SIDE

COLOR SPECIFICATIONS

- FACE: 3/16" #7328 White acrylic
- RETURN: .063" aluminum painted Total Red (PMS 2035C), satin finish; reflective white interior surface
- TRIM CAP: 1" Red Jewelite
- BACK: .177" bluish tint polycarbonate with vinyl applied
- BAFFLE: .080" pre-coated white aluminum
- FILM: 3M Translucent Film #3630-236 Turquoise applied around perimeter of cabinet back
- LED: White LED modules; 6500K
- Aluminum Backer Painted Total Red (PMS 2035C)



NIGHT VIEW

PROPOSED SIGNAGE

SCALE PROPORTIONALLY

32-10

INTELLECTUAL PROPERTY OF:

M3 GRAPHICS
PRINT • SIGNS • LED • T-SHIRTS
281-933-3000
www.M3Graphics.us

COMPANY NAME / PROJECT NAME

Total Wireless

ADDRESS

200 W Jefferson Blvd
Dallas, TX 75208

CHANNEL LETTERS SPECIFICATIONS

- Dual Lit Channel Letters with LED Lights
 - 3/16" Plexiglass face
 - Pre-finished Aluminum .063 Gage
 - 3" Returns Painted
 - 1" Black Jewelite face trim
 - 3/8" x 5" Galvanized Bolts with anchors
 - Letters with Single Load
 - Transformers 120 Vol.
 - Primary voltage 12 VCD/2AMPS/.24KVA
- POWER SUPPLY IS NOT OVERLOADED

PROJECT MANAGER:
AARON VALVERDE

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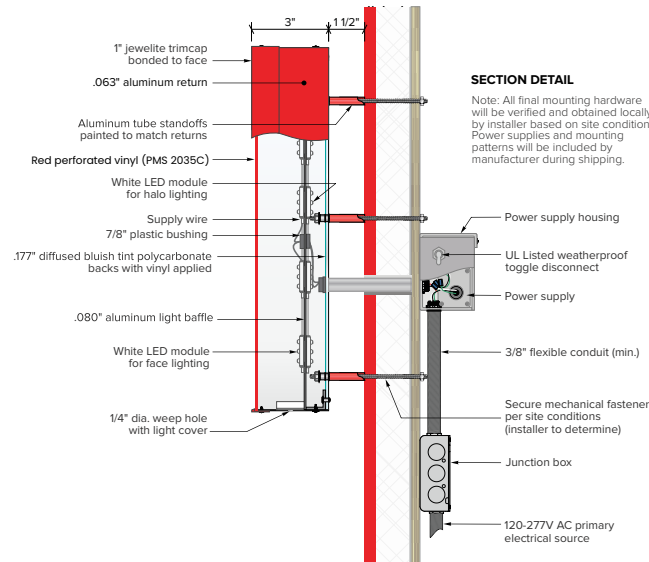
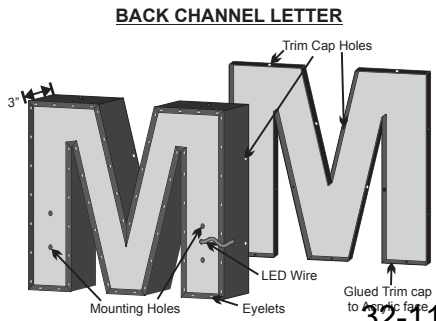
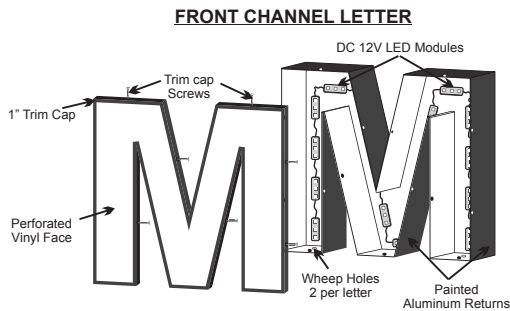
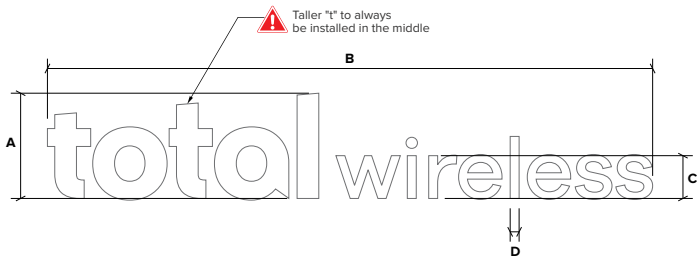
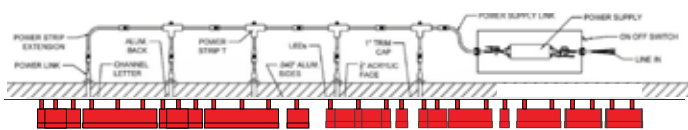
METHOD OF ATTACHMENT

Dual Lit channel letters mounted on an aluminum panel with separators

SIDE



ELECTRICAL LOAD:
 1amps @ 12V DC / .5amps @12V DC
 TOTAL letters = 60 watts
 wireless letters = 96 watts
 Total 156 watt



COLOR SPECIFICATIONS

- FACE: 3/16" #7328 White acrylic
- RETURN: .063" aluminum painted Total Red (PMS 2035C), satin finish; reflective white interior surface
- TRIM CAP: 1" Red Jewelite
- BACK: .177" bluish tint polycarbonate with vinyl applied
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COMPANY NAME / PROJECT NAME

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ADDRESS

200 W Jefferson Blvd
 Dallas, TX 75208

CHANNEL LETTERS SPECIFICATIONS

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 - 3/8" x 5" Galvanized Bolts with anchors
 - Letters with Single Load
 - Transformers 120 Vol.
 - Primary voltage 12 VCD/2AMPS/.24KVA
- POWER SUPPLY IS NOT OVERLOADED

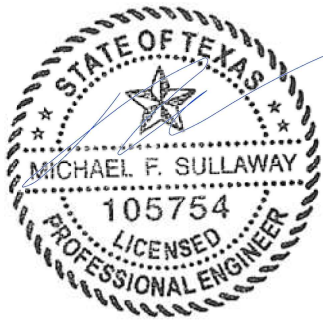
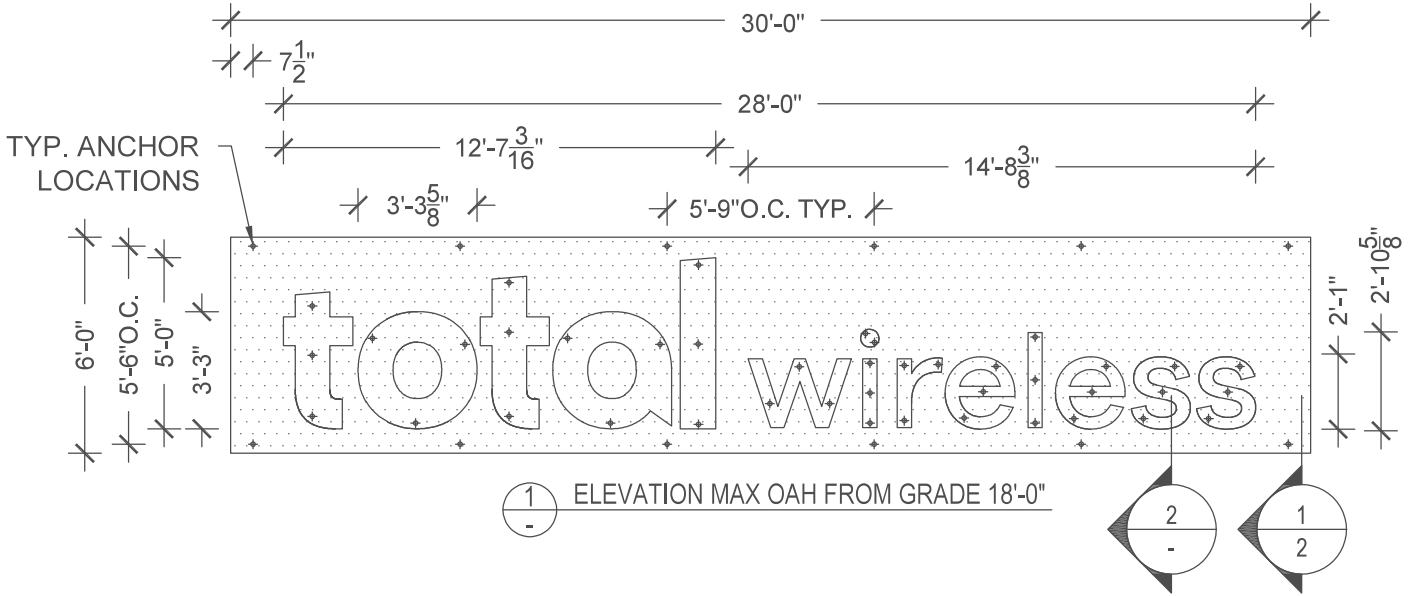
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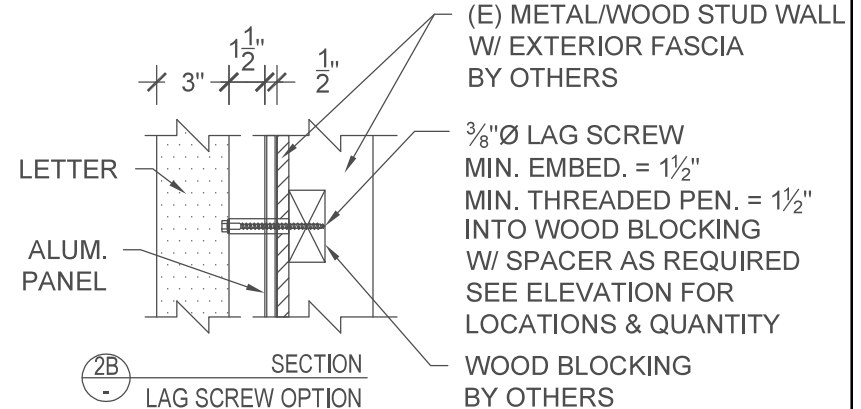
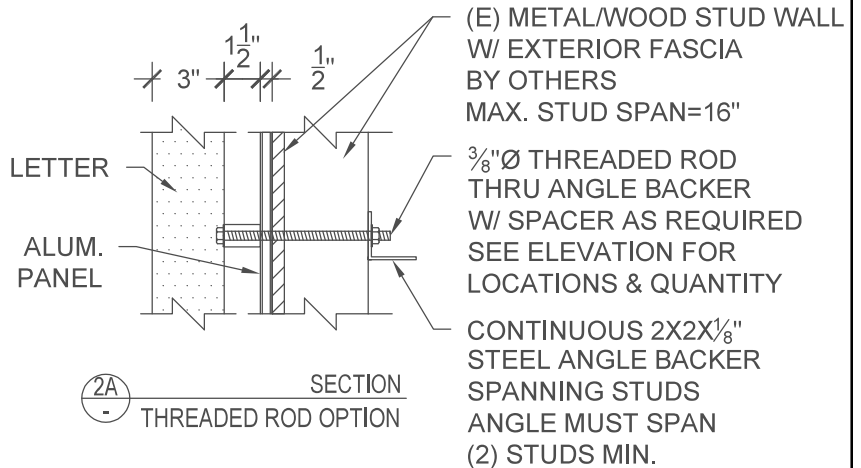
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PROJECT: TOTAL WIRELESS, 200 W. JEFFERSON BLVD., DALLAS, TX
PROJECT #: 56001
CLIENT: M3 GRAPHICS

DATE: 03/21/2026
ENGINEER: PRC
LAST REVISED:



CERTIFICATE OF AUTHORITY
NO. F-14143
3/25/2026

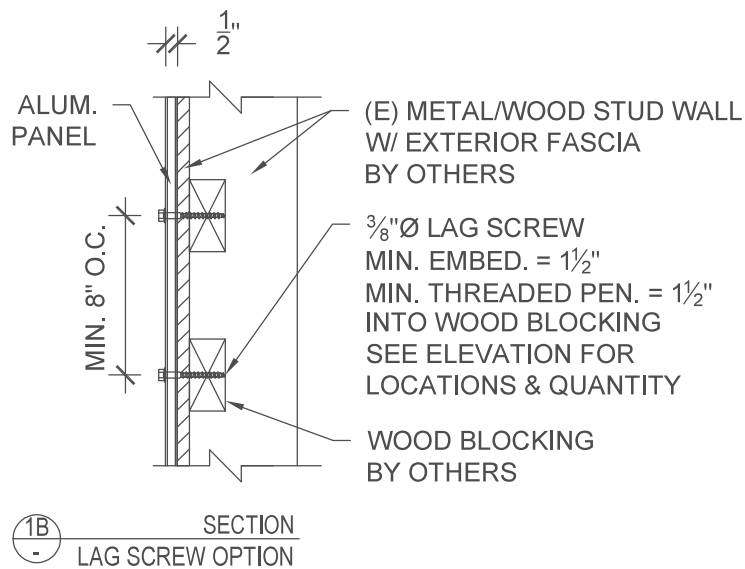
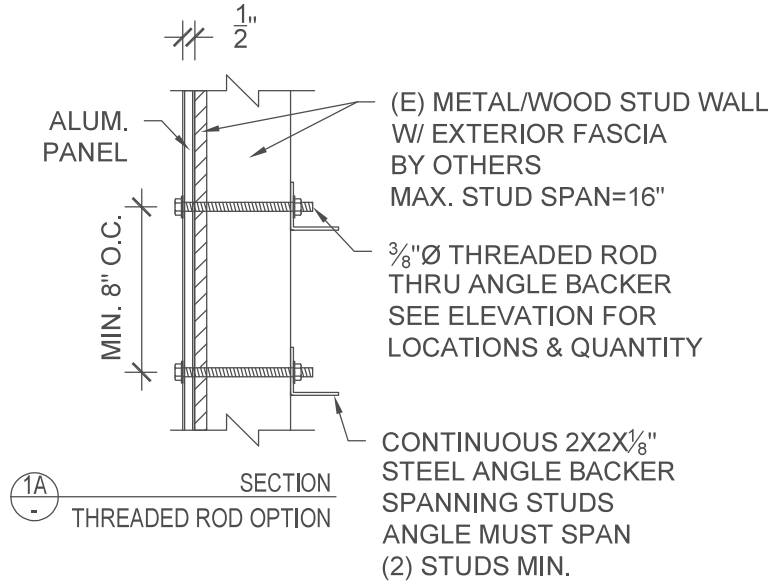


GENERAL NOTES

- DESIGN CODE: IBC 2021
- DESIGN LOADS: ASCE 7-16
- WIND VELOCITY 105 MPH EXPOSURE C
- THREADED ROD STEEL ASTM A36, Fu = 58 KSI MIN.
- LAG SCREWS PER NDS SPECIFICATIONS
- ANGLE STEEL ASTM A36, Fy = 36 KSI MIN.
- ALL EXISTING ELEMENTS AND DIMENSIONS TO BE VERIFIED IN FIELD
- ALL DIMENSIONS SHOWN TO BE VERIFIED PRIOR TO FABRICATION

PROJECT: TOTAL WIRELESS, 200 W. JEFFERSON BLVD., DALLAS, TX
PROJECT #: 56001
CLIENT: M3 GRAPHICS

DATE: 03/21/2026
ENGINEER: PRC
LAST REVISED:



CERTIFICATE OF AUTHORITY
NO. F-14143
3/25/2026



PROJECT: TOTAL WIRELESS
 PROJ. NO.: 56001
 CLIENT: M3 GRAPHICS

DATE: 03/21/2026
 ENGINEER: PRC

V5.8

units: pounds, feet unless noted otherwise

Applied Wind Loads; from ASCE 7-16

$p_{net} = \lambda K_{zt} p_{net30}$	(ASCE 30.4-1)	
$\lambda = 1.21$	(ASCE Fig. 30.4-1)	
$K_{zt} = 1.0$	(unless unusual landscape)	
$V = 105$ mph	Exposure =	c
Area = 1.60 ft ²		
max. height = 18.00 ft		
$p_{net30} = 19.84$ psf		$p_{net} = 24.01$ psf
$p_{net30} = -26.59$ psf		$p_{net} = -32.18$ psf

THREADED ROD OPTION

Check 0.375" Dia. Threaded Rod Steel - Alum. Panel to Wall (LRFD:)

$\phi = 0.75$

Pnet =	See Above =	32.18 psf
Tributary Area =	$A_{Trib} = (5-9") * (3'-0") =$	17.25 ft ²
Wind Load =	$WL = Pnet * ATrib =$	0.555 kips
Dead Load =	$DL = 1.2 * 10psf * ATrib =$	0.207 kips
#bolts =	=	1 bolt
Tu =	$WL / \#bolts =$	0.555 kips (Governs)
Vu =	$DL / \#bolts =$	0.207 kips (Governs)
dia. =	=	0.375 in
Abolt =	=	0.110 in ²
Fnt =	$(58ksi * 0.75) =$	43.50 ksi
Fnv =	$(58ksi * 0.45) =$	26.10 ksi
$\phi Tn =$	$\phi * Fnt * Abolt =$	3.603 kips OK
$\phi Vn =$	$\phi * Fnv * Abolt =$	2.162 kips OK

Combined Check

Fv =	$Vu / Abolt =$	1.874 ksi
$F'nt =$	$1.3Fnt - Fnt * Fv / \phi Fnv \leq Fnt =$	43.50 ksi
$\phi Tn =$	$\phi * Fnt * Abolt =$	3.603 kips OK

LAG SCREW OPTION

Check Loads on 0.375" Dia. Lag Screws - Alum. Panel to Wall (LRFD:)

$\phi = 0.75$

(WL/DL See Above)	Tu =	$WL / \#bolts =$	0.555 kips (Governs)
	Vu =	$DL / \#bolts =$	0.207 kips (Governs)



PROJECT: TOTAL WIRELESS
 PROJ. NO.: 56001
 CLIENT: M3 GRAPHICS

DATE: 03/21/2026
 ENGINEER: PRC

V5.8

units: pounds, feet unless noted otherwise

THREADED ROD OPTION

Check 0.375" Dia. Threaded Rod Steel - Letters to Alum. Panel (LRFD:)

$\phi = 0.75$

Pnet=	See Above=	32.18 psf	
Tributary Area per Letter "O"=	$A_{Trib}=(3'-3.625")*(3'-3")=$	10.73 ft ²	
Wind Load=	WL=Pnet*ATrib=	0.345 kips	
Dead Load=	DL=1.2*10psf*ATrib=	0.107 kips	
arm(DL)=	(3'')/2+(1.5'')+(0.5'')=	3.5 in	
MDL=	DL*arm=	0.376 k-in	
Min. Spacing(DL)=	Sd=	8 in	
Additional tension due to DL=	TDL=MDL/Sd/1 bolt=	0.047 kips	
#bolts=	=	3 bolts	
Tu=	WL/#bolts +TDL=	0.162 kips	
Vu=	DL/#bolts=	0.036 kips	
dia.=	=	0.375 in	
Abolt=	=	0.110 in ²	
Fnt=	(58ksi*0.75)=	43.50 ksi	
Fnv=	(58ksi*0.45)=	26.10 ksi	
$\phi Tn=$	$\phi *Fnt*Abolt=$	3.603 kips	OK
$\phi Vn=$	$\phi *Fnv*Abolt=$	2.162 kips	OK

Combined Check

Fv=	Vu/Abolt=	0.324 ksi	
F'nt=	$1.3Fnt-Fnt*Fv/\phi Fnv \leq Fnt=$	43.50 ksi	
$\phi Tn=$	$\phi *Fnt*Abolt=$	3.603 kips	OK

LAG SCREW OPTION

Check Loads on 0.375" Dia. Lag Screws - Letters to Alum. Panel (LRFD:)

$\phi = 0.75$

(WL/DL See Above)	Tu=	WL/#bolts +TDL=	0.162 kips
	Vu=	DL/#bolts=	0.036 kips



PROJECT: TOTAL WIRELESS DATE: 03/21/2026
 PROJ. NO.: 56001 ENGINEER: PRC
 CLIENT: M3 GRAPHICS

(ALUM. PANEL)

LAG SCREWS (LRFD) - SOLID WOOD TO SOLID ALUMINUM - WITHDRAWAL AND SINGLE SHEAR LATERAL

DESIGN INPUT	FACTORED FASTENER LOADING		MAIN MEMBER		SIDE MEMBER	
	W_u	555 lb	Withdrawal Load	DOUGLAS FIR-LARCH		ALUMINUM
Z_u	207 lb	Lateral Load	G	0.5	F_u	42 ksi Ultimate Strength
FASTENER DIMENSIONS			t_m	1.5 in	t_s	0.063 in Thickness
L_m	1.5 in	Length into Main MBR	θ	90 deg		
D	0.375 in	Nominal Diameter				
w	0 in	Washer				
g	0 in	Gap				

P_{min} 1.5 in Minimum dowel penetration for lateral loading [NDS 11.1.3.7]
 p 1.5 in Actual dowel penetration based on selected dowel length

STANDARD HEX LAG SCREWS [NDS Appendix Table L2]

D_r	0.265 in	D	0.25	0.313	0.375	0.438	0.5	0.625	0.75	0.875	1	1.125	1.25	
F_{yb}	45000 psi	[NDS Table I1]	D_r	0.173	0.227	0.265	0.328	0.371	0.471	0.579	0.683	0.78	0.887	1.012

DOWEL BEARING CALCULATIONS

$F_{e, }$	5600 psi				Dowel bearing strength, perpendicular to grain [NDS Table 11.3.2 Footnote 2]
$F_{e,perp}$	3646.03 psi				Dowel bearing strength, parallel to grain [NDS Table 11.3.2 Footnote 2]
F_{em}	3646.03 psi	F_e	63000 psi		Dowel bearing strength - Hankinson formula [NDS 11.3-11] & Steel [NDS Comm. 12]
L_m	1.5 in	L_s	0.063 in		Dowel bearing length
q_m	966.199 lbs/in	q_s	16695 lbs/in		Dowel bearing resistance [AWC Technical Report 12] - D_r Assumption
M_m	139.572 in-lbs	M_s	139.572 in-lbs		Dowel moment resistance based [AWC Technical Report 12] - D_r Assumption

YIELD MODE DOWEL EQUATIONS [AWC Technical Report 12 Table 1-1]

I_m	289.86 lb	P	1449.3			R_d	5	K_D	3.15	θ	90		
I_s	210.357 lb	P	1051.79			R_d	5	K_D	3.15	K_θ	1.25		
II	131.852 lb	P	593.334	A	3E-04	B	0.782	C	-560.05	R_d	4.5	K_D	3.15
III_m	178.583 lb	P	714.33	A	3E-04	B	0.75	C	-683.06	R_d	4	K_D	3.15
III_s	128.185 lb	P	512.74	A	5E-04	B	0.032	C	-156.14	R_d	4	K_D	3.15
IV	178.52 lb	P	714.078	A	5E-04	B	0	C	-279.14	R_d	4	K_D	3.15

Z 128.185 lb Ref Value
 Z' 276.879 lb Adj Value

Adjustment Factors [NDS Table 10.3.1]

C_M	C_t	C_g	C_Δ	C_d	C_{eg}	C_{st}	C_{di}	C_{tn}	K_F	ϕ	λ
1	1	1	1		1		1	1	3.32	0.65	1

WITHDRAWAL LOADING [NDS 11.2.1]

W	304.966 lb/in	Reference Value [NDS 11.2-1]
W'	658.726 lb/in	Adj Value
$p_{t,req}$	0.84264 in	Required thread penetration for withdrawal
$p_{t,req}$	0.875 in	-->Rounded up to nearest 1/8"
$p_{t,ovr}$	1.5 in	Override for additional thread penetration
$p_{t,sel}$	1.50 in	

Adjustment Factors [NDS Table 10.3.1]

C_M	C_t	C_{eg}	K_F	ϕ	λ
1	1	1	3.32	0.65	1

COMBINED LATERAL AND WITHDRAWAL LOADING [NDS 11.4.1]

α 1.21385 rad = 69.548 deg
 Z_u' 592.412 lb
 Z_α' 752.189 lb Based on $p_{t,sel}$
 RATIO 0.788 PASS



PROJECT: TOTAL WIRELESS DATE: 03/21/2026
 PROJ. NO.: 56001 ENGINEER: PRC
 CLIENT: M3 GRAPHICS

(LETTERS)

LAG SCREWS (LRFD) - SOLID WOOD TO SOLID ALUMINUM - WITHDRAWAL AND SINGLE SHEAR LATERAL

DESIGN INPUT	FACTORED FASTENER LOADING		MAIN MEMBER		SIDE MEMBER	
	W_u	162 lb	Withdrawal Load	DOUGLAS FIR-LARCH		ALUMINUM
Z_u	36 lb	Lateral Load	G	0.5	F_u	42 ksi
FASTENER DIMENSIONS			t_m	1.5 in	t_s	0.063 in
L_m	1.5 in	Length into Main MBR	θ	90 deg		Ultimate Strength
D	0.375 in	Nominal Diameter				Thickness
w	0 in	Washer				
g	2 in	Gap				

Main Member End Grain (x)

p_{min} 1.5 in Minimum dowel penetration for lateral loading [NDS 11.1.3.7]
 p 1.5 in Actual dowel penetration based on selected dowel length

STANDARD HEX LAG SCREWS [NDS Appendix Table L2]

D_f	0.265 in	D	0.25	0.313	0.375	0.438	0.5	0.625	0.75	0.875	1	1.125	1.25	
F_{yb}	45000 psi	[NDS Table I1]	D_r	0.173	0.227	0.265	0.328	0.371	0.471	0.579	0.683	0.78	0.887	1.012

DOWEL BEARING CALCULATIONS

$F_{e, }$	5600 psi														Dowel bearing strength, perpendicular to grain [NDS Table 11.3.2 Footnote 2]
$F_{e,perp}$	3646.03 psi														Dowel bearing strength, parallel to grain [NDS Table 11.3.2 Footnote 2]
F_{em}	3646.03 psi	F_e	63000 psi												Dowel bearing strength - Hankinson formula [NDS 11.3-11] & Steel [NDS Comm. 12]
L_m	1.5 in	L_s	0.063 in												Dowel bearing length
q_m	966.199 lbs/in	q_s	16695 lbs/in												Dowel bearing resistance [AWC Technical Report 12] - D_r Assumption
M_m	139.572 in-lbs	M_s	139.572 in-lbs												Dowel moment resistance based [AWC Technical Report 12] - D_r Assumption

YIELD MODE DOWEL EQUATIONS [AWC Technical Report 12 Table 1-1]

I_m	289.86 lb	P	1449.3						R_d	5	K_D	3.15	θ	90
I_s	210.357 lb	P	1051.79						R_d	5	K_D	3.15	K_θ	1.25
II	43.8912 lb	P	197.51	A	3E-04	B	2.782	C	-560.05	R_d	4.5	K_D	3.15	
III_m	60.5564 lb	P	242.226	A	3E-04	B	2.75	C	-683.06	R_d	4	K_D	3.15	
III_s	18.8424 lb	P	75.3695	A	5E-04	B	2.032	C	-156.14	R_d	4	K_D	3.15	
IV	33.6531 lb	P	134.612	A	5E-04	B	2	C	-279.14	R_d	4	K_D	3.15	

Z 18.8424 lb Ref Value
 Z' 40.6995 lb Adj Value

Adjustment Factors [NDS Table 10.3.1]

C_M	C_t	C_G	C_Δ	C_d	C_{eg}	C_{st}	C_{di}	C_{tn}	K_F	ϕ	λ
1	1	1	1		1		1	1	3.32	0.65	1

WITHDRAWAL LOADING [NDS 11.2.1]

W	304.966 lb/in	Reference Value [NDS 11.2-1]
W'	658.726 lb/in	Adj Value
$p_{t,req}$	0.24602 in	Required thread penetration for withdrawal
$p_{t,req}$	0.250 in	-->Rounded up to nearest 1/8"
$p_{t,ovr}$	1.5 in	Override for additional thread penetration
$p_{t,sel}$	1.500 in	

Adjustment Factors [NDS Table 10.3.1]

C_M	C_t	C_{eg}	K_F	ϕ	λ
1	1	1	3.32	0.65	1

COMBINED LATERAL AND WITHDRAWAL LOADING [NDS 11.4.1]

α	1.35354 rad = 77.552 deg
Z_u'	165.962 lb
Z_α'	474.702 lb Based on $p_{t,sel}$
RATIO	0.350 PASS



PROJECT: TOTAL WIRELESS
 PROJ. NO.: 56001
 CLIENT: M3 GRAPHICS

DATE: 03/21/2026
 ENGINEER: PRC

units; pounds, feet unless noted otherwise

Check L2X2X1/8 for flexure (geometric axes) (AISC 14 F10)

	$M_x = T_u \cdot 16''/4 =$	2.22 k-in (Tu See Page #3)	$F_y =$	36 ksi
	$M_y = V_u \cdot 16''/4 =$	0.828 k-in (Vu See Page #3)	$S_x =$	0.129 in ³
Yielding:			$S_y =$	0.129 in ³
	$M_{nx} = 1.5M_y = 1.5 F_y S_x =$	6.966 k-in (eq'n. F10-1)	$E =$	29000 ksi
	$M_{ny} = 1.5M_x = 1.5 F_x S_y =$	6.966 k-in (eq'n. F10-1)	$b =$	2 in
LTBx:			$d =$	2 in
	$M_e = 0.66E b^4 t C_b / L_b^2 ((1+0.78(L_b t/b^2)^2)^{1/2} - 1) =$	15.88 k-in (eq'n. F10-6a)	$t =$	0.125 in
	$M_e = 0.66E b^4 t C_b / L_b^2 ((1+0.78(L_b t/b^2)^2)^{1/2} + 1) =$	356.8 k-in (eq'n. F10-6b)	$C_b =$	1.14
	$M_e > M_y$ Therefore:		$L_b =$	16 in
	$M_n = (1.92 - 1.17 \sqrt{M_y/M_e}) \cdot M_y =$	6.0 k-in (eq'n. F10-3)	$\phi =$	0.9
LTBy:				
	$M_e = 0.66E d^4 t C_b / L_b^2 ((1+0.78(L_b t/d^2)^2)^{1/2} - 1) =$	16 k-in (eq'n. F10-6a)		
	$M_e = 0.66E d^4 t C_b / L_b^2 ((1+0.78(L_b t/d^2)^2)^{1/2} + 1) =$	356.8 k-in (eq'n. F10-6b)		
	$M_e > M_y$ Therefore:			
	$M_n = (1.92 - 1.17 \sqrt{M_y/M_e}) \cdot M_y =$	6.0 k-in (eq'n. F10-3)		
LLBx:				
	$M_n = F_y S_c (2.43 - 1.72(b/t)(F_y/E)^{1/2}) =$	5.426 k-in (eq'n. F10-7)	$S_{cx} =$	0.103 in ³
LLBy:				
	$M_n = F_y S_c (2.43 - 1.72(b/t)(F_y/E)^{1/2}) =$	5.426 k-in (eq'n. F10-7)	$S_{cy} =$	0.103 in ³
	$\phi M_{nx} =$	4.9 k-in OK		
	$\phi M_{ny} =$	4.9 k-in OK		
	$M_x / \phi M_{nx} + M_y / \phi M_{ny} =$	0.624 < 1 OK		